Serial No. 10/762,559 Docket No. K06-165935M/TBS

# **AMENDMENTS TO THE CLAIMS:**

#### Please amend the claims as follows:

1. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft <u>comprising</u>: <del>comprising, on the basis of mass%;</del>

C: 0.45<u>wt%</u> - 0.55<u>wt</u>% C; [[,]]

Si: 0.10wt% - 0.50wt% Si; [[,]]

Mn: 0.50wt% - 1.20wt% Mn; [[,]]

P: 0.025wt% or less P; [[,]]

S: 0.025wt% or less S: [[,]]

Mo: 0.15wt% - 0.25wt% Mo; [[,]]

B: 0.0005wt% - 0.005wt% B; [[,]]

Ti: 0.005wt% - 0.010wt% Ti; , and

N:  $0.015\underline{\text{wt}}\%$  or less  $\underline{\text{N}}$ ; [[,]] satisfying the following relations 1 and 2 and

the balance comprising Fe and inevitable impurities: impurities.

#### Relation 1

wherein  $0.80 \le \text{Ceq} \le 0.95$ , where  $\text{Ceq} = \text{C} + 0.07 \times \text{Si} + 0.16 \times \text{Mn} + 0.20 \times \text{Cr} + 0.72 \times \text{Mo}$ , and

# Relation 2

wherein f value  $\leq 1.0$ , where f value =  $1.78 - 3.2 \times C + 0.05 \times Si - 0.60 \times Mn - 0.55 \times Cu - 0.80 \times Ni - 0.75 \times Cr_{\underline{.}}$ 

(Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim
wherein <u>further comprising</u> one or more of <u>Cu</u>: 0.50<u>wt</u>% or less <u>Cu</u>, <u>Ni</u>: 0.50<u>wt</u>% or less <u>Ni</u>

described above.

Docket No. K06-165935M/TBS

and Cr: 0.50wt% or less Cr is contained instead of a portion of the balance of said Fe

3

3. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim 1, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less <u>Ta</u>, Zr: 0.10wt% or less <u>Zr</u> and Al: 0.10wt% or less <u>Al</u> is contained instead of a portion of the balance of said Fe described above.

4. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim 2, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less <u>Ta</u>, Zr: 0.10wt% or less <u>Zr</u> and Al: 0.10wt% or less <u>Al</u> is contained instead of a portion of the balance of <u>said</u> Fe described above.

5. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft <u>comprising</u>: <del>comprising, on the basis of mass%;</del>

C: 0.45wt% - 0.55wt% C; [[,]]

Si: 0.10wt% - 0.50wt% Si; [[,]]

Mn: 0.50wt% - 1.20wt% Mn; [[,]]

P: 0.025wt% or less P; [[,]]

<u>S</u>: 0.025<u>wt</u>% or less <u>S</u>; [[,]]

Mo: 0.15wt% - 0.25wt% Mo; [[,]]

B: 0.0005wt% - 0.005wt% B; [[,]]

Ti: 0.005wt% - 0.010wt% Ti; , and

N: 0.015wt% or less N; [[,]] satisfying the following relations 1 and 2 and the balance comprising Fe and inevitable impurities: impurities.

Docket No. K06-165935M/TBS

in which the tissue wherein the steel after hot rolling is comprises a 3-phase texture of ferrite + pearlite + bainite,

wherein the ferrite area ratio is 40% or less,

and wherein the maximum pearlite block size is 100 µm or less in a circle-equivalent diameter,

wherein the hardness after hot rolling is 24 to 30 HRC,

wherein the surface hardness after high frequency hardening is 650 HV or higher, and wherein the old austenite crystal grain size in the hardened layer is 8 or more in view of grain size number[[;]].

### Relation 1

wherein  $0.80 \le \text{Ceq} \le 0.95$ , where  $\text{Ceq} = \text{C} + 0.07 \times \text{Si} + 0.16 \times \text{Mn} + 0.20 \times \text{Cr} + 0.72 \times \text{Mo}$ , and

#### Relation 2

wherein f value  $\leq 1.0$ , where f value =  $1.78 - 3.2 \times C + 0.05 \times Si - 0.60 \times Mn - 0.55 \times Cu - 0.80 \times Ni - 0.75 \times Cr$ .

- 6. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim 5, wherein <u>further comprising</u> one or more of <u>Cu</u>: 0.50<u>wt</u>% or less <u>Cu</u>, <u>Ni</u>: 0.50<u>wt</u>% or less <u>Ni</u> and <u>Cr</u>: 0.50<u>wt</u>% or less <u>Cr</u> is contained instead of a portion of the balance of <u>said</u> Fe described above.
- 7. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim 5, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less <u>Ta</u>, Zr: 0.10wt% or less <u>Zr</u> and Al: 0.10wt% or less <u>Al</u> is contained instead of a portion of the balance of <u>said</u> Fe described above.

Docket No. K06-165935M/TBS

8. (Currently Amended) A steel for use in <u>a</u> high strength pinion shaft according to claim 6, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less Ta, Zr: 0.10wt% or less Zr and Al: 0.10wt% or less Al is contained instead of a portion of the balance of <u>said</u> Fe described above.

9. (Currently Amended) A method of manufacturing a steel for use in <u>a</u> high strength pinion shaft in which a steel <u>comprising</u>: <del>comprising</del>; <del>comprising</del>; on the basis of mass%;

C: 0.45wt% - 0.55wt% C; [[,]]

Si: 0.10wt% - 0.50wt% Si; [[,]]

Mn: 0.50wt% - 1.20wt% Mn; [[,]]

P: 0.025wt% or less P: [[,]]

S: 0.025 wt% or less S; [[,]]

Mo: 0.15wt% - 0.25wt% Mo; [[,]]

B: 0.0005wt% - 0.005wt% B; [[,]]

Ti: 0.005wt% - 0.010wt% Ti; , and

N: 0.015wt% or less N; [[,]] satisfying the following relations 1 and 2 and the balance comprising Fe and inevitable impurities: impurities, is fabricated or worked under a draft ratio at an area reduction of 10% or more, and at a temperature of 850°C or lower: lower,

## Relation 1

wherein  $0.80 \le \text{Ceq} \le 0.95$ , where  $\text{Ceq} = \text{C} + 0.07 \times \text{Si} + 0.16 \times \text{Mn} + 0.20 \times \text{Cr} + 0.72 \times \text{Mo}$ , and

## Relation 2

Docket No. K06-165935M/TBS

wherein f value  $\leq 1.0$ , where  $T_{Tr} = 2.78 - 3.2 \times C + 0.05 \times Si - 0.60 \times Mn - 0.55 \times Cu - 0.80 \times Ni - 0.75 \times Cr$ .

6

- 10. (Currently Amended) A method of manufacturing a steel for use in <u>a</u> high strength pinion shaft according to claim 9, wherein <u>further comprising</u> one or more of <u>Cu</u>: 0.50<u>wt</u>% or less <u>Cu</u>, <u>Ni</u>: 0.50<u>wt</u>% or less <u>Ni</u> and <u>Cr</u>: 0.50<u>wt</u>% or less <u>Cr</u> is contained instead of a portion of the balance of said Fe described above.
- 11. (Currently Amended) A method of manufacturing a steel for use in <u>a</u> high strength pinion shaft according to claim 9, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less Ta, Zr: 0.10wt% or less Zr and Al: 0.10wt% or less Al is contained instead of a portion of the balance of said Fe described above.
- 12. (Currently Amended) A method of manufacturing a steel for use in <u>a</u> high strength pinion shaft according to claim 10, wherein <u>further comprising</u> one or more of Nb: 0.20wt% or less Nb, Ta: 0.20wt% or less Ta, Zr: 0.10wt% or less Zr and Al: 0.10wt% or less Al is eontained instead of a portion of the balance of said Fe described above.
- 13. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein a ferrite ratio of said steel comprises 40% or less.
- 14. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein a hardness of said steel after hot rolling comprises a range of 24 HRC to 30 HRC.

0. 10//02,339

Docket No. K06-165935M/TBS

15. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein a surface hardness of said steel comprises 650 HV or more.

7

- 16. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein said steel comprises an old austenite crystal grain size of 8 or more.
- 17. (New) A method of manufacturing a steel for use in <u>a</u> high strength pinion shaft according to claim 9, wherein said steel is fabricated or work under a temperature in a range of 700°C to 850°C.
- 18. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein a torsional strength of said steel comprises 1670 Mpa to 1800 Mpa.
- 19. (New) A steel for use in a high strength pinion shaft according to claim 1, wherein a wear loss of said steel comprises 0.002g to 0.004g.